# Design of an ultrafiltration unit

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# Outline



2 Cleaning cycle

# Objectives

- Poiseuilli Flow
   Navier Stokes Equation
- 5 D'Arcy's Law: Porous Media

#### 6 Conclusion

Cleaning cycle Objectives Poiseuilli Flow D'Arcy's Law: Porous Media Conclusion

# 1 The filter

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#### The filter Cleaning cycle Objectives Poiseuilli Flow

# Filter

#### • One of the uses of the filter is to purify water.

- Within the cartridge there are about 3000 hollow fibres made of plastic foam with radius 330 $\mu$ .
- The foam is a porous material(pores with radius 0.1µ). This enables pure water to flow through the pores while filtering the small particles out.
- Impure water is pumped into the system at high pressure (100 kPa).
- The pure water moves almost radially though the porous foam. The pressure function found in the foam can be found by using D'Arcy's Law.
- Then the pure water moves axially along the lumen. Using Poiseuille Flow, one can find the velocity of the water. Hence, the flux.
- The water will then be gathered at the end of the cartridge.

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## **Filtration Process**



# The filter

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- During filtration, waste accumulates and some even smaller particles get lodged into the pores.
- To clean the fibres, a high pressured (500-700kPa), short duration air pulse is sent through the lumen. Thus clearing the pores.



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- Find the expression for the flux through each lumen in terms of the length inner and outer radii.
- Determine how important parameters give maximum flux.



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Navier Stokes Equation

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Navier Stokes Equation

## Poiseuilli Flow

#### Poiseuilli Flow

Poiseuille flow- The steady flow of an incompressible fluid parallel to the axis of a circular pipe of infinite length, produced by a pressure gradient along the pipe.

Navier Stokes Equation

# Fibres



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Navier Stokes Equation

# Navier Stokes Equation

• Navier Stokes Equation

$$\frac{\partial \vec{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \vec{v} = \frac{1}{\rho} \nabla \rho + \mu \nabla^2 \vec{v} + \vec{F}$$
(1)

Incompressibility condition for fluid

$$\nabla \cdot \vec{v} = 0 \tag{2}$$

Navier Stokes Equation

• Velocity of fluid along the lumen

$$\vec{u} = (u_r, u_\theta, u_z)$$
(3)  
= (0, 0, u\_z(r)) (4)

- From Navier-Stokes equation, three components in cylindrical are obtained:
- *r* component :  $\frac{\partial p}{\partial r} = 0$
- $\theta$  component : 0 = 0
- *z*-component:  $\frac{dp}{dz} = \frac{\mu}{r} \frac{d}{dr} (r \frac{du}{dr})$

Navier Stokes Equation

• Boundary condition:

$$r = r_0, u_z(r_0) = 0$$
 (5)

• The resulting velocity is given as :

$$u_{z} = \frac{(r^{2} - r_{0}^{2})}{4\mu} \frac{dp}{dz}$$
(6)

Navier Stokes Equation

• Flux = volume of fluid entering a cross-section area

$$Q = \int_0^{r_0} 2\pi r u_z \,\mathrm{d}r \tag{7}$$

$$Q = -\frac{\pi r_0^4}{8\mu} \frac{dp}{dz}$$
(8)

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# D'Arcy Flow

#### D'Arcy's Law

states that the average volumetric discharge of flow through a porous medium is directly proportional to the hydraulic gradient assuming that the flow is laminar and inertia can be neglected.

$$v_r = -\frac{k}{\mu}\vec{\nabla}p \tag{9}$$

where

K is the hydraulic permeability  $(2 \times 10^{-16} m^2)$ 

 $\mu$  is the dynamic viscosity(1x10<sup>-3</sup>Pa sec of water)

 $\underline{v}$  is the volume flux/area

# Longitudinal section of Fibres



# Cross-section of Fibres



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## Cross-section area

- From the figure above we get that  $dA = 2\pi r v_r$
- Due to the Continuity equation

$$\nabla \cdot (\nabla p) = 0 \tag{10}$$

• Expanding this in cylindrical coordinates gives:

$$\frac{1}{r}\frac{d}{dr}\left(r\frac{dp}{dz}\right) = 0 \tag{11}$$

Integrating we get

$$p_r = A \ln r + B \tag{12}$$

where

$$A = \frac{p_0 - p_1}{\ln(\frac{r_0}{r_1})} = 0, B = P_1$$
(13)

• Boundary Conditions:

$$r = r_0 \Longrightarrow p = p_0 \tag{14}$$

$$r = r_1 \Longrightarrow p = p_1 \tag{15}$$

• where  $p_1$  is a constant along the lumen and  $p_0$  is a constant in a cross-section.

Finding the pressure in the porous medium using D'Arcy's law

• Now consider D'Arcy's law

$$V(r) = \frac{k}{\mu} P_r \tag{16}$$

• Let q(z) = total flux/length going into the lumen at a chosen cross-section.

$$q(z) = 2\pi r V(r) = constant$$
(17)

$$= -2\pi \frac{k}{\mu} A \tag{18}$$

• Therefore 
$$q(z) = \left(\frac{2\pi k}{\mu} \frac{1}{\ln(\frac{r_0}{r_1})}\right)(p_0 - p_1)$$
  
• Let  $\xi = \frac{2\pi k}{\mu} \frac{1}{\ln(\frac{r_0}{r_1})}$ 

# Section 3

• Summary of the reuslts from Poiseulli flow and Darcy's law gives :

$$Q_z(z) = q(z) \tag{19}$$

$$q(z) = -(p_1 - p(z))\xi$$
 (20)

$$Q(z) = -\gamma \frac{dp}{dz} \tag{21}$$

• where  $\gamma = \frac{\pi r_1^4}{8\mu}$  and  $p_0$  is no longer a constant but a function p(z) that varies along the lumen.

• Differentiate (15) and equating the results with (14) gives:

$$\frac{d^2p}{dz^2} - \vec{\Gamma}p(z) = -p_1\vec{\Gamma}$$
(22)

where  $\vec{\Gamma} = \frac{\xi}{\gamma}$ • Boundary Conditions

$$z = 0, \frac{dp}{dz} = 0$$

$$z = L, p = p_0 \tag{24}$$

(23)

• Pressure in the lumen : 
$$p = p_1 - (p_0 - p_1) rac{cosh(z\sqrt{ec{r}})}{cosh(L\sqrt{ec{r}})}$$

## Pressure



## Pressure gradient



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• Corresponding flux in the lumen:

$$Q(z) = \frac{pir_1^4}{8\mu} \frac{dp}{dz}$$
(25)

$$=\frac{\vec{\Gamma}r_{1}^{4}}{8\mu}\left((p_{0}-p_{1})\frac{\sinh(\sqrt{\vec{\Gamma}}z)}{\cosh(L\sqrt{\vec{\Gamma}})}\right)$$
(26)

• At z = L the flux is defined as follows:

$$Q(L) = \frac{\vec{\Gamma} r_1^4}{8\mu} \left[ (p_0 - p_1) tanh(\sqrt{\vec{\Gamma}} L) \right]$$
(27)

# Total Flux



## Rate of change of total flux



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# Flux and inner radius versus fixed length



## Flux and inner radius versus length



# Filtration cycle



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- Problem reduction
- Identified effect of salient parameters
- Used determined effect to understand how to meet specifications of filtration unit



# Thank You!!!

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# AND HAPPY BIRTHDAY DZANGA!!!

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